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# Current experimental compressor investigations – a short overview

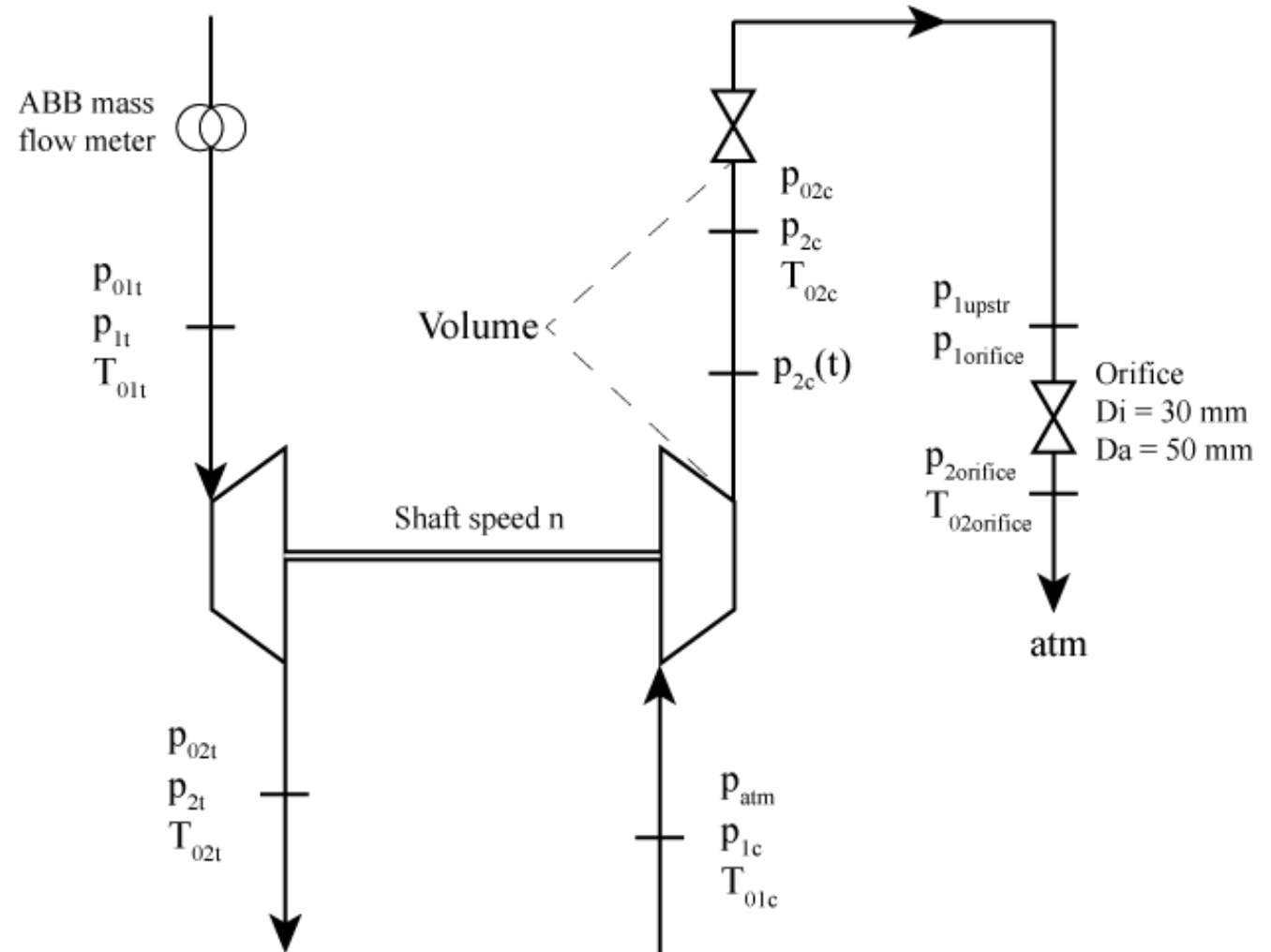
Bertrand Kerres

# Research questions

- Hurst exponent as a criterion for compressor surge
- Effect of bended inlet on compressor performance at low mass flows
- Impeller flow recirculation

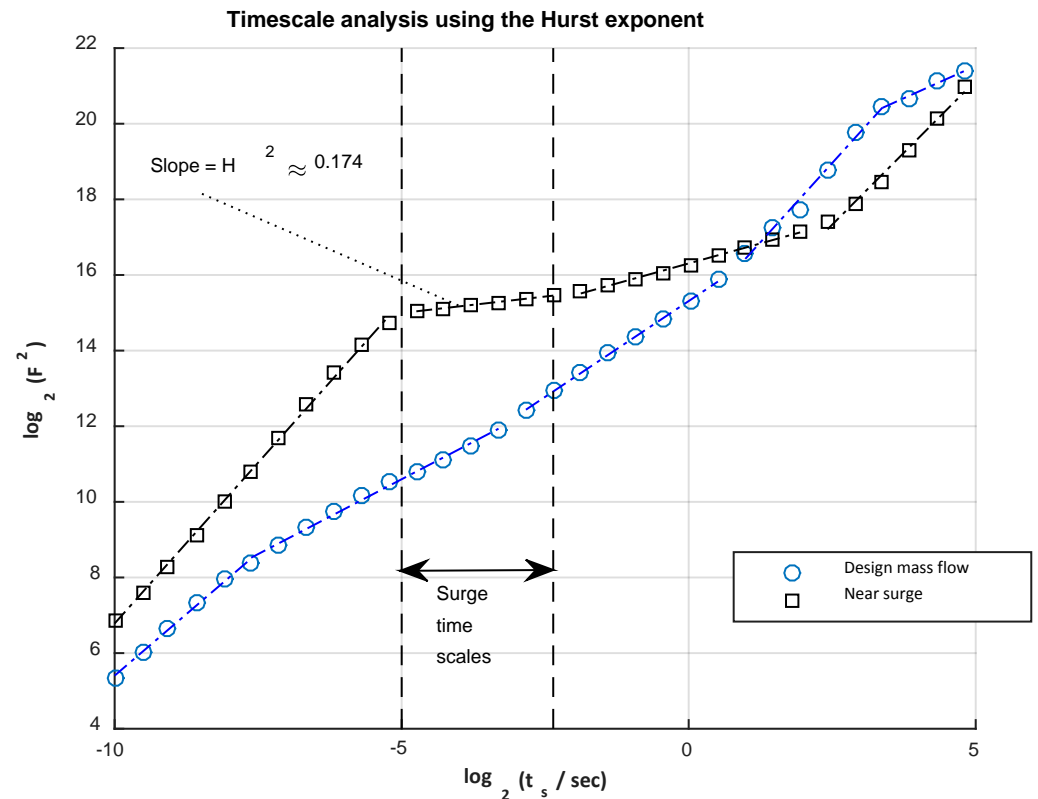
# Experimental setup

- GT1752 turbocharger (6+6 blades, TRIM = 0.53)
- Cold gas stand
- Orifice for mass flow measurements (accurate, but no oscillations)
- Relatively small volume between compressor and throttle (approx. 1 L)



# The Hurst exponent as an indicator of compressor surge

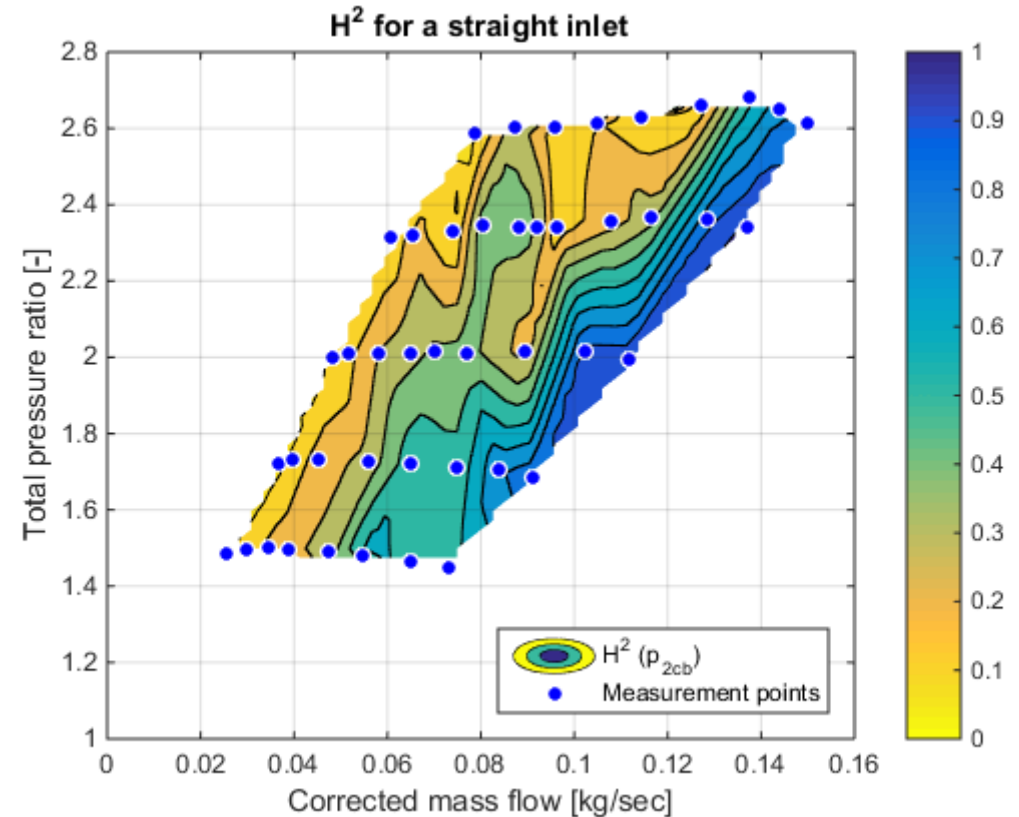
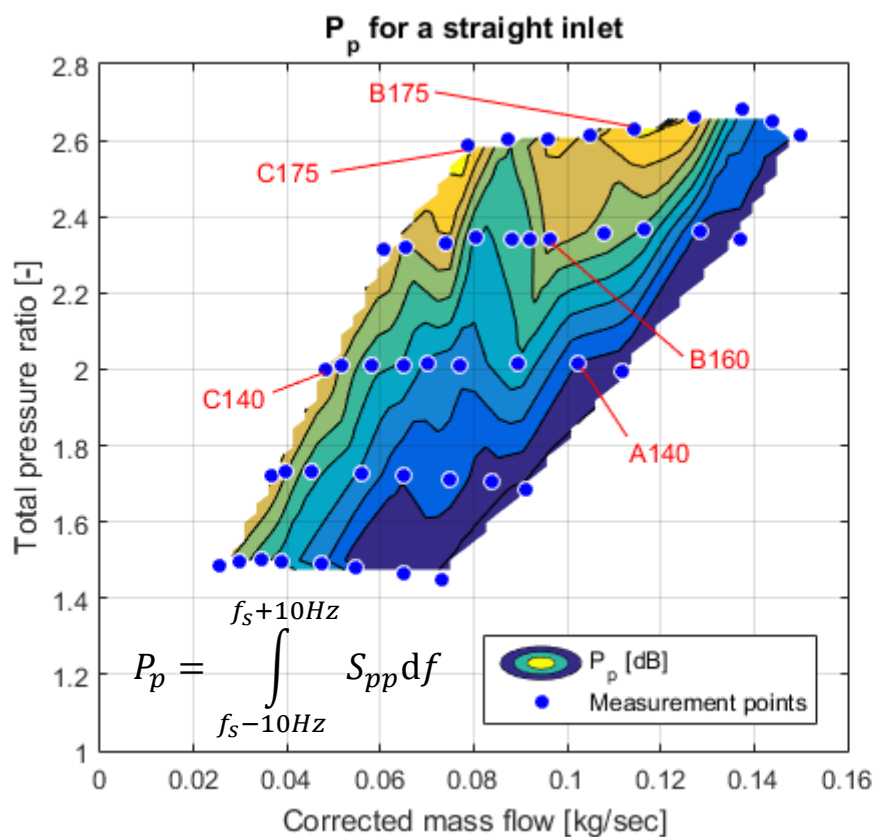
- Hurst exponent  $H^2$ : non-dimensional number that gives information about correlations and long-term trends in a time series
- $H^2 = 0 \dots 0.5$  : Negatively correlated
- $H^2 = 0.5$ : White noise
- $H^2 = 0.5 \dots 1$ : Positively correlated
- $H^2 > 1$ : Non-stationary
- Compressor surge pressure signal is anti-correlated in the surge time scales  $\rightarrow H^2 \approx 0$



Kerres, B., Kabral, R., Nair, V., and Åbom, M., The Hurst Exponent as an Indicator of Turbocharger Compressor Surge, manuscript in preparation (ASME J Turbomachinery)

Kerres, B., Nair, V., Cronhjort, A., and Mihaescu, M., Analysis of the Turbocharger Compressor Surge Margin Using a Hurst-Exponent-based Criterion, submitted to SAE world congress 2016

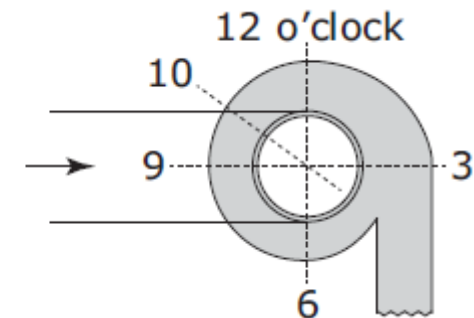
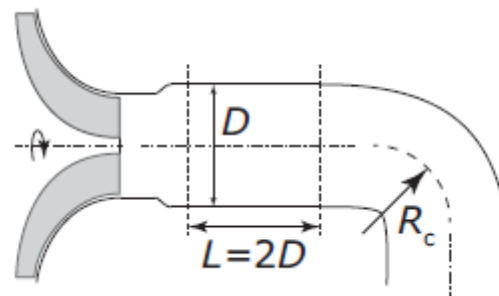
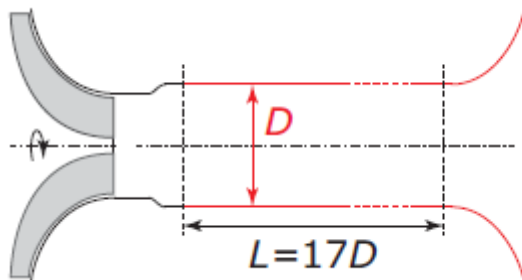
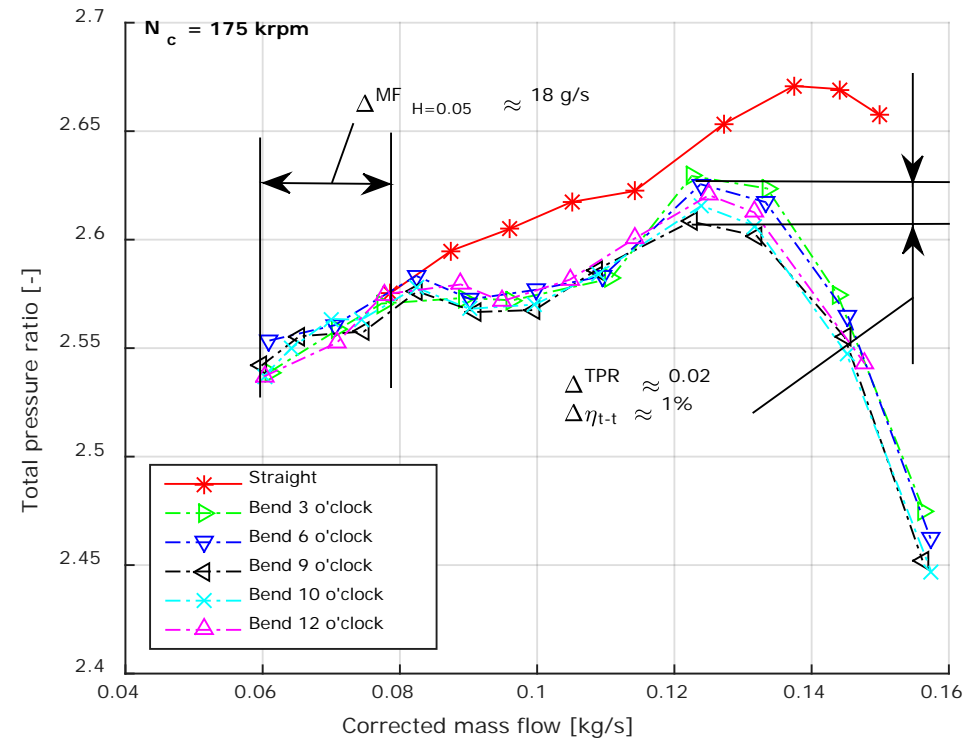
# Comparison: Spectral Power vs $H^2$ for Straight Inlet



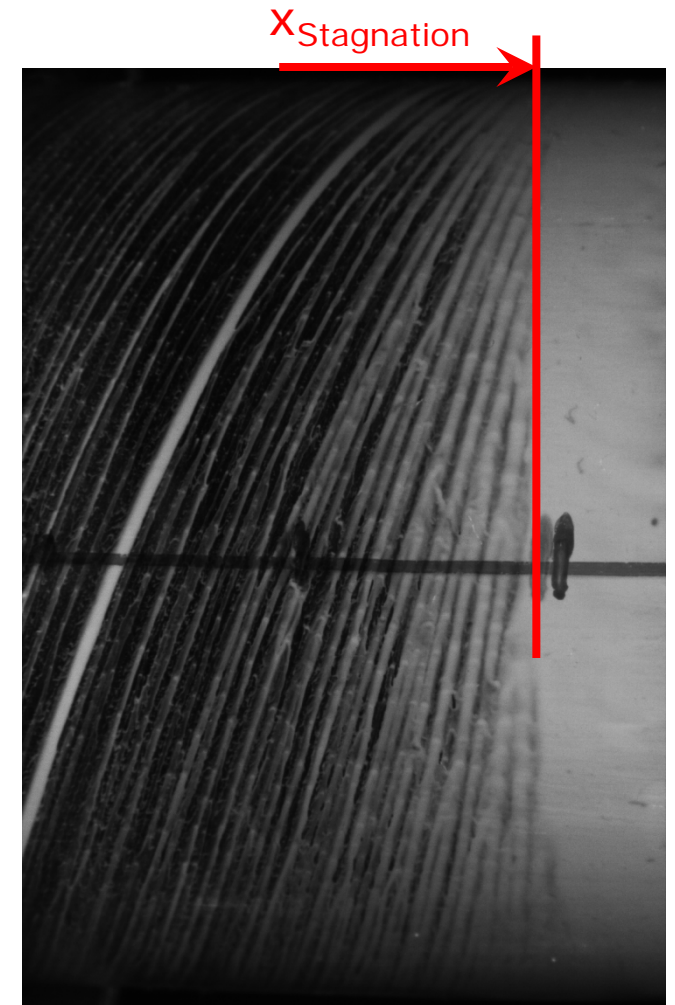
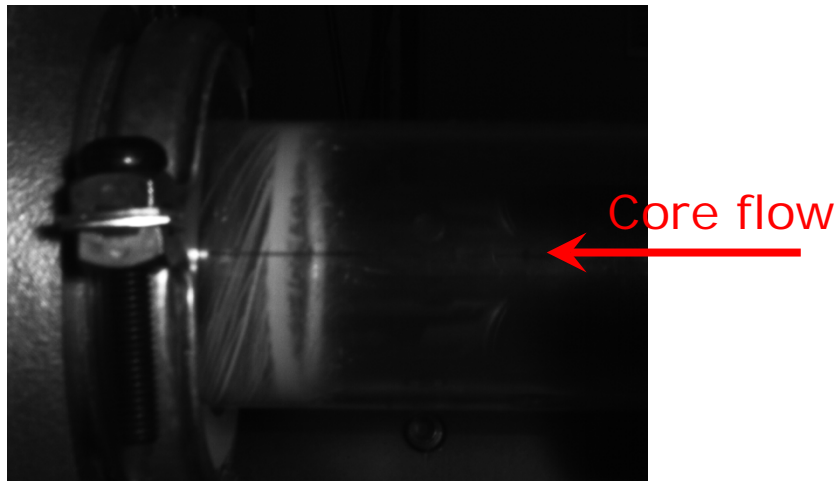
- +  $H^2$  has a clear limit for surge, which is system-independent ( $H^2 \rightarrow 0$ )
- +  $H^2$  is more sensitive to small amplitude oscillations  $\rightarrow$  could be better for detection of surge pre-cursors
- $H^2$  is computationally (much) more expensive

# Effect of bended inlet on compressor performance

- Inlet geometries:
  - Straight
  - Bend (different orientations)
- Results:
  - Lower pressure ratio (TPR) due to bend losses
  - Bend gives an increase in surge margin at high impeller speeds (value depends on surge threshold)
  - Orientation slightly affects TPR



# Impeller flow recirculation



- Visualize wall streamlines from the impeller backflow using Zinkoxide + oil
- Experimental data can be used to validate CFD simulations (and evtl. inlet blockage models)
- Flow angle of the backflow can be estimated
- Gain understanding of the flow field if there is an angle upstream

# Outlook

- Impeller flow recirculation
- Switch to BorgWarner compressor (start of 2016)
  - Inlet geometry tests
  - Rotating stall detection using pressure transducers (diff. circumferential / radial positions)
- Engine tests





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Thank You!

# Estimating the Hurst Exponent Using Detrended Fluctuation Analysis

- Here: artificial sample signals  $x(t)$

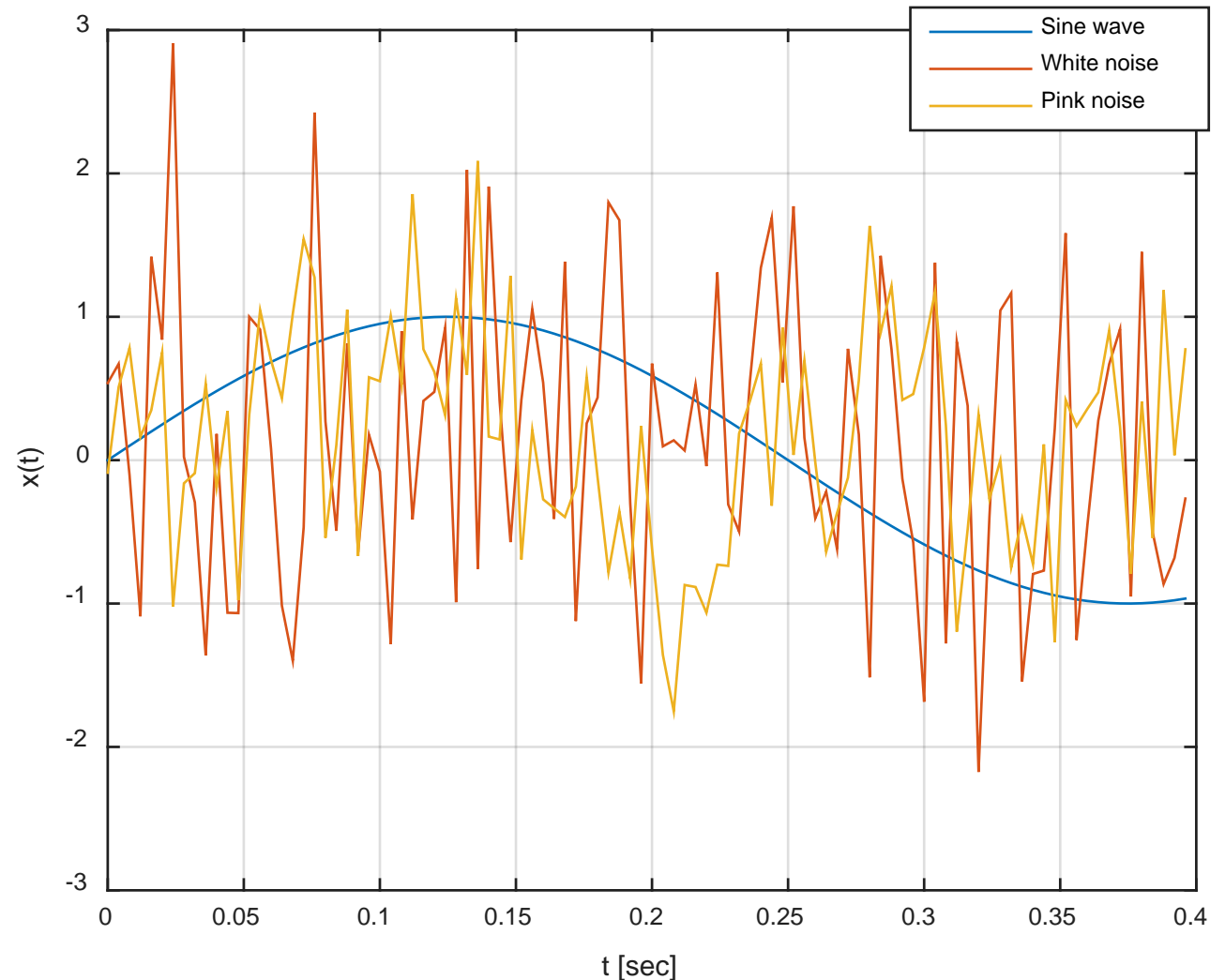
Sine wave (signal power  $S$  contained in 1 frequency):

$$x_s = \sin(\omega t)$$

White noise (signal power  $S$  independent of frequency):

$$x_w \sim \mathcal{N}(0,1)$$

Pink noise (signal power  $S \sim 1/f$ )



# Estimating the Hurst Exponent

- Using Detrended Fluctuation Analysis (DFA)
- (Simplified) method:
  - Calculate cumulative series
 
$$Y = \sum x_i$$
  - For different time scales  $t_s$ :
    - Split into windows with length  $t_s$
    - Remove window linear trend
    - Calculate window variance
    - Calculate root mean of window variances (thus  $H^2$ )
  - Plot log-log diagram  $t_s$  – root mean ( $Y$ )
  - Fit a linear trend  $\rightarrow$  Slope is the Hurst exponent

